

SAB2223 Mechanics of Materials and Structures

TOPIC 9 TORSION

Lecturer:

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OPENCOURSEWARE

TOPIC 9 TORSION

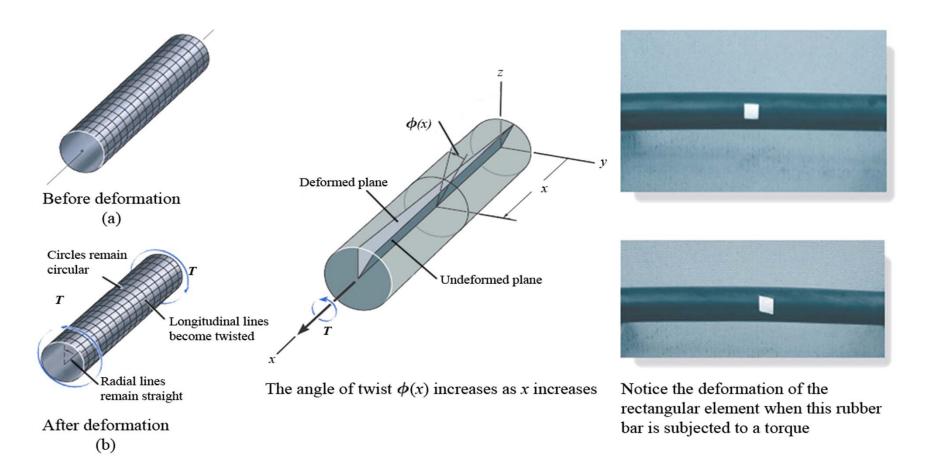






Torsion Formula

- Two assumptions:
 - Linear and elastic deformation
 - Plane section remains plane and undistorted





Torsion Formula

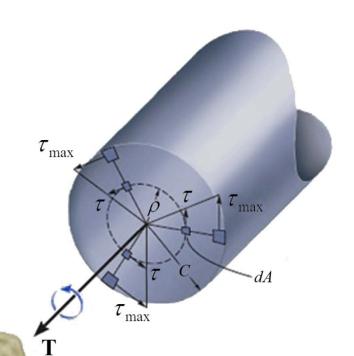
- Linear distribution of stress: $\tau = \frac{\rho}{c} \tau_{\text{max}}$
- Torsion shear relationship:

$$T = \int_{A} \rho(\tau) dA = \int_{A} \rho\left(\frac{\rho}{c}\right) \tau_{\text{max}} dA$$

$$T = \frac{\tau_{\text{max}}}{c} \int_{A} \rho^{2} dA$$

$$au_{
m max} = \frac{Tc}{J}$$

$$\tau = \frac{T\rho}{J}$$



Shear stress varies linearly along each radial line of the cross section



Torsion Formula

– Solid shaft:

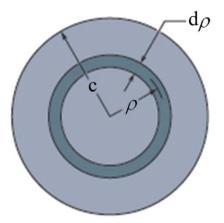
$$J = \int_{A} \rho^{2} dA = \int_{0}^{C} \rho^{2} (2\pi \rho d\rho) = 2\pi \int_{0}^{C} \rho^{3} d\rho = 2\pi \left(\frac{1}{4}\right) \rho^{4} \Big|_{0}^{C}$$

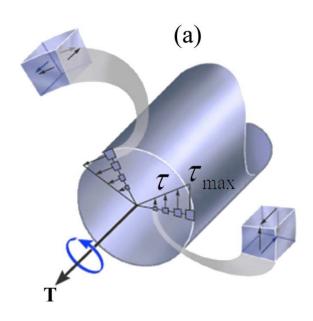
$$J = \frac{\pi}{2}c^4$$

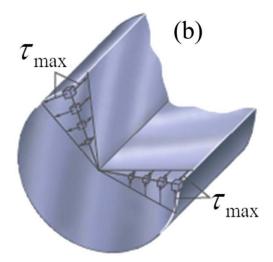
– Tubular shaft:

$$J = \frac{\pi}{2} \left(c_o^4 - c_i^4 \right)$$

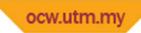
$$J = \frac{\pi}{2} \left(c_o^4 - c_i^4 \right)$$







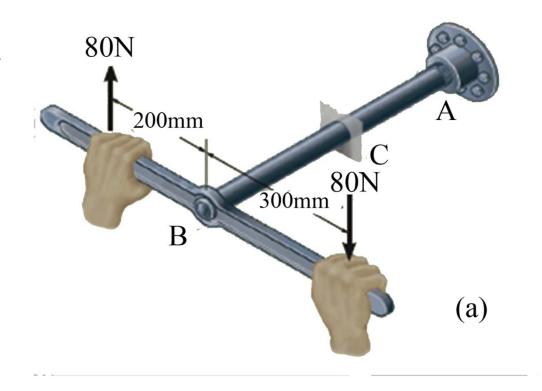
Shear stress varies linearly along each radial line of the cross section





Example 1

The pipe shown has an inner diameter of 80 mm and an outer diameter of 100 mm. If its end is tightened against the support at A using a torque wrench at B, determine the shear stress developed in the material at the inner and outer walls along the central portion of the pipe when the 80-N forces are applied to the wrench.





Example 1 (cont.)

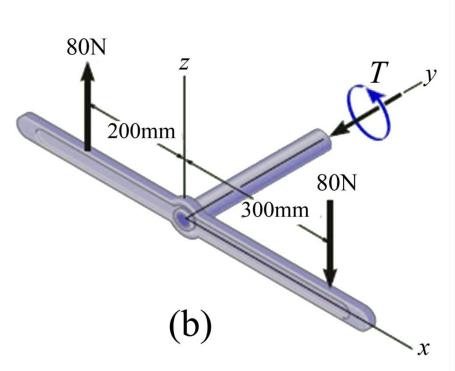
$$\sum M_y = 0;$$

80(0.3)+80(0.2-T)=0
 $T = 40 \text{ N} \cdot \text{m}$

$$J = \frac{\pi}{2} \left[(0.05)^4 - (0.04)^4 \right] = 5.796 \left(10^{-6} \right) \text{m}^4$$

$$\rho = c_0 = 0.05 \text{ m}$$

$$\tau_0 = \frac{Tc_0}{J} = \frac{40(0.05)}{5.796(10^{-6})} = 0.345 \text{ MPa}$$

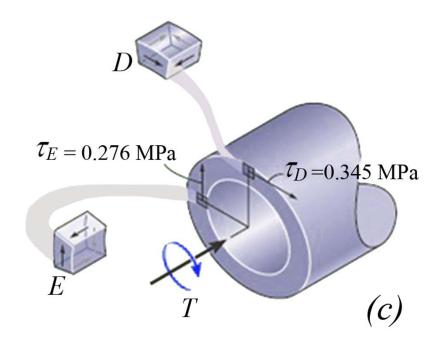




Example 1 (cont.)

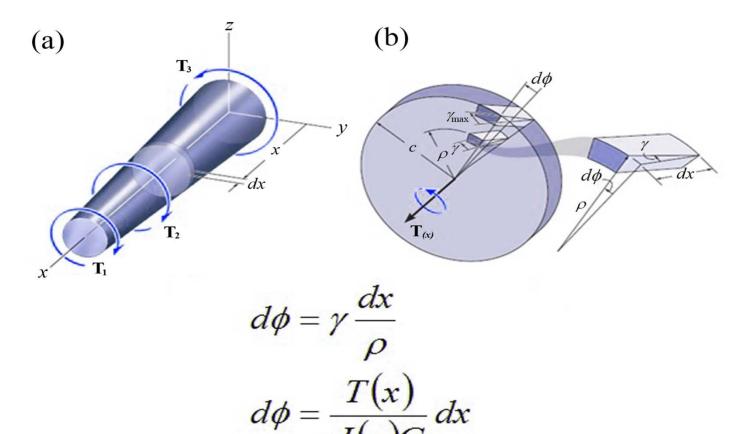
$$\rho = c_i = 0.04 \,\mathrm{m}$$

$$\tau_i = \frac{Tc_i}{J} = \frac{40(0.04)}{5.796(10^{-6})} = 0.276 \text{ MPa}$$





Angle of Twist



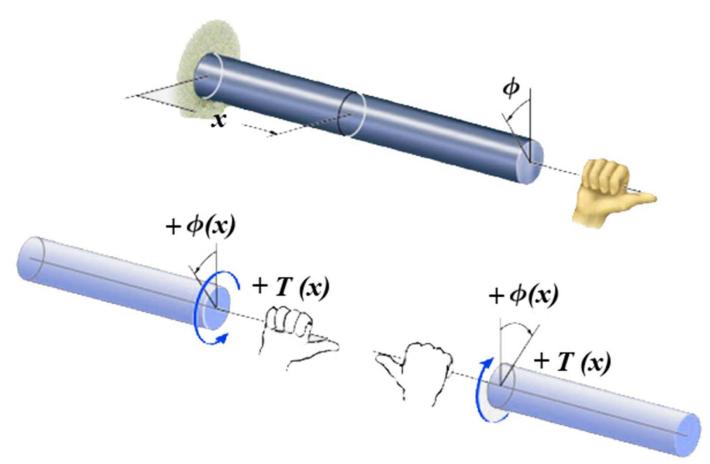
For constant torque and cross-sectional area:

$$\phi = \frac{TL}{JG}$$



Angle of Twist

• Sign convention:



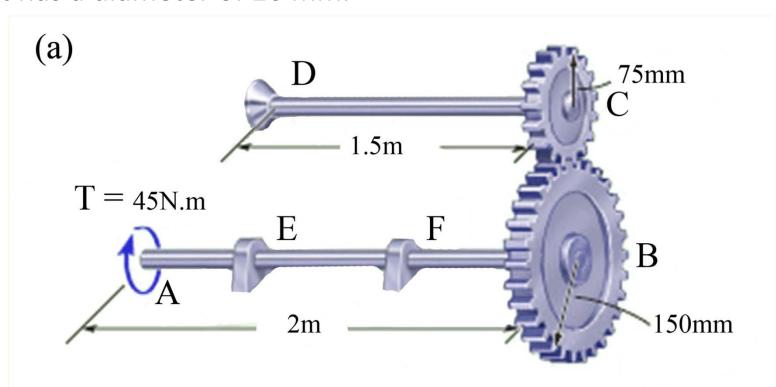
Positive sign convention for T and ϕ





Example 2

The two solid steel shafts are coupled together using the meshed gears. Determine the angle of twist of end A of shaft AB when the torque 45 Nm is applied. Take G to be 80 GPa. Shaft AB is free to rotate within bearings E and F, whereas shaft DC is fixed at D. Each shaft has a diameter of 20 mm.

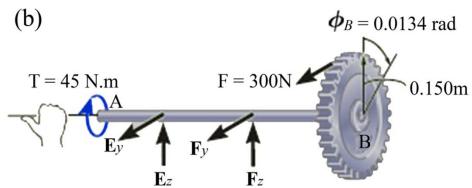




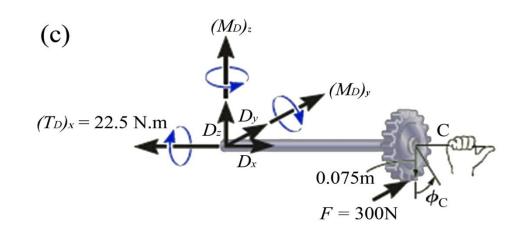
Example 2 (cont.)

$$F = 45/0.15 = 300 \text{ N}$$

 $(T_D)_x = 300(0.075) = 22.5 \text{ Nm}$



$$\varphi_C = \frac{TL_{DC}}{JG} = \frac{(+22.5)(1.5)}{(\pi/2)(0.001)^4 \lceil 80(10)^9 \rceil} = +0.0269 \text{ rad}$$



$$\varphi_B(0.15) = (0.0269)(0.075) \Rightarrow 0.0134 \text{ rad}$$





Example 2 (cont.)

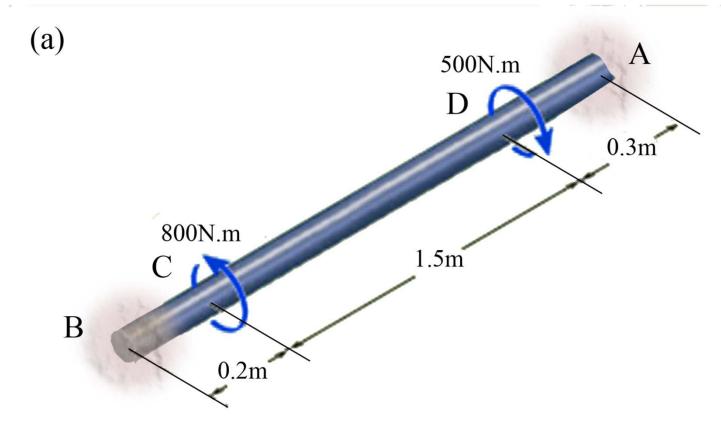
$$\varphi_{A/B} = \frac{T_{AB}L_{AB}}{JG} = \frac{(+45)(2)}{(\pi/2)(0.010)^4 \left[80(10^9)\right]} = +0.0716 \text{ rad}$$

$$\varphi_A = \varphi_B + \varphi_{A/B} = 0.0134 + 0.0716 = +0.0850 \text{ rad}$$





The solid steel shaft shown below has a diameter of 20 mm. If it is subjected to the two torques, determine the reactions at the fixed supports A and B.



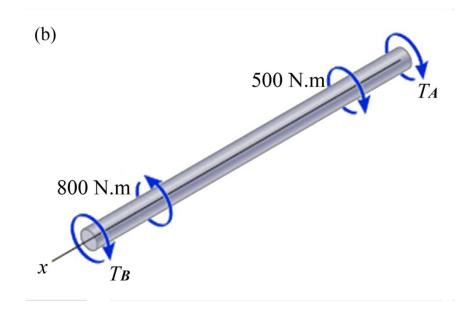


Example 3 (cont.)

$$\sum M_x = 0$$

$$-T_b + 800 - 500 - T_A = 0 \qquad (1)$$

$$\phi_{A/B} = 0$$



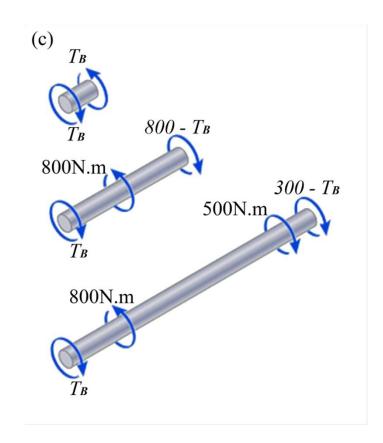


Example 3 (cont.)

$$\frac{-T_B(0.2)}{JG} + \frac{(800 - T_B)(1.5)}{JG} + \frac{(300 - T_B)(0.3)}{JG} = 0$$

$$T_B = 645 \text{ N} \cdot \text{m}$$

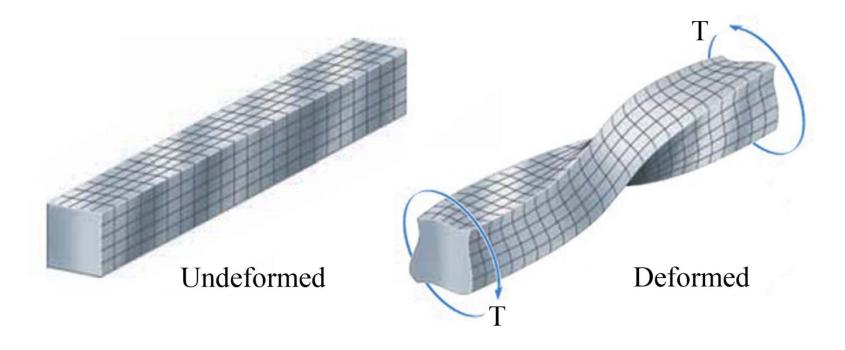
$$T_A = -345 \,\mathrm{N} \cdot \mathrm{m}$$

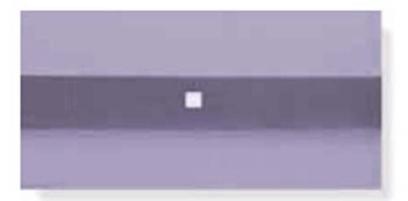


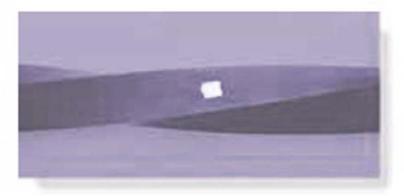




Solid Non-Circular Shafts









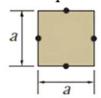
Solid Non-Circular Shafts

Shape of cross section

 $\tau_{\rm max}$

 ϕ

Square



 $\frac{4.81 \ T}{a^3}$

 $\frac{7.10\ TL}{a^4G}$

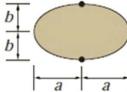
Equilateral triangle



 $\frac{20.7}{2^3}$

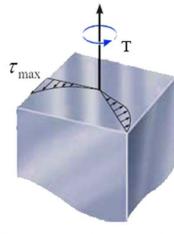
 $\frac{46\ TL}{a^4G}$





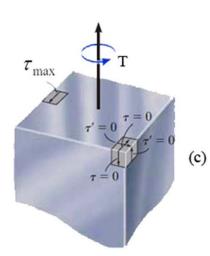
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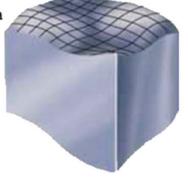
 $\frac{(a^2+b^2)TI}{\pi a^3b^3G}$



(a) Shear stress distribution along two radial lines

(b) Warping of cross-sectional area



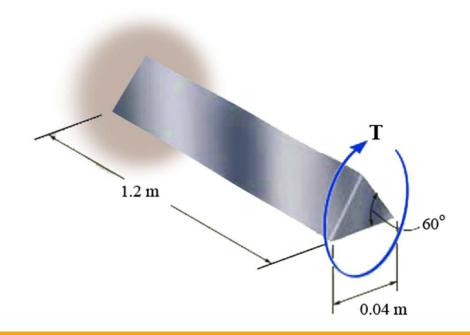






Example 4

The 6061-T6 aluminum shaft shown below has a cross-sectional area in the shape of an equilateral triangle. Determine the largest torque **T** that can be applied to the end of the shaft if the allowable shear stress is $t_{allow} = 56$ MPa. and the angle of twist at its end is restricted to $\Phi_{allow} = 0.02$ rad. How much torque can be applied to a shaft of circular cross section made from the same amount of material?

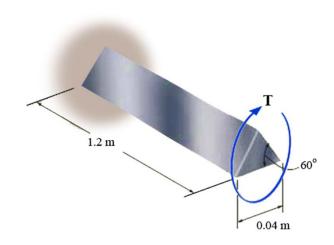




Example 4 (cont.)

$$\tau_{allow} = \frac{20T}{a^3};$$
 $56 = \frac{20T}{40^3} \Rightarrow T = 1779.2 \text{ Nm}$

$$\sigma_{allow} = \frac{46T}{a^4 G_{al}};$$
 $0.02 = \frac{46T (1.2)(10^3)}{40^4 [26(10^3)]} \Rightarrow T = 24.12 \text{ Nm}$





Example 4 (cont.)

$$A_{circle} = A_{triangle}; \quad \pi c^2 = \frac{1}{2} (40) (40 \sin 60^\circ) \Rightarrow c = 14.85 \text{ mm}$$

$$\tau_{allow} = \frac{Tc}{J}; \quad 56 = \frac{T(14.85)}{(\pi/2)(14.85)^4} \Rightarrow T = 288.06 \text{ Nm}$$

$$\varphi_{allow} = \frac{TL}{JG_{al}}; \quad 0.02 = \frac{T(1.2)(10^3)}{(\pi/2)(14.85)^4 [26(10^3)]} \Rightarrow T = 33.10 \text{ Nm}$$



Thin Wall Tubes Having Closed Section

Average shear stress

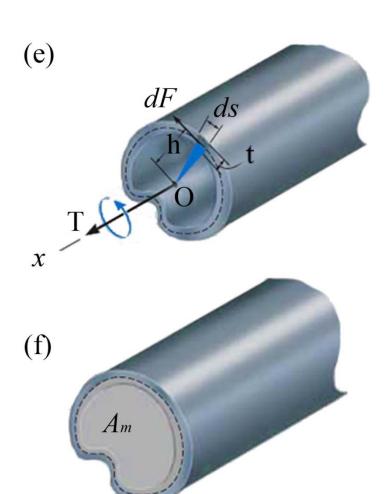
$$\tau_{avg} = \frac{T}{2tA_m}$$

Shear flow

$$q = \frac{T}{2A_m}$$

Angle of twist

$$\varphi = \frac{TL}{4A_m^2G} \oint \frac{ds}{t}$$



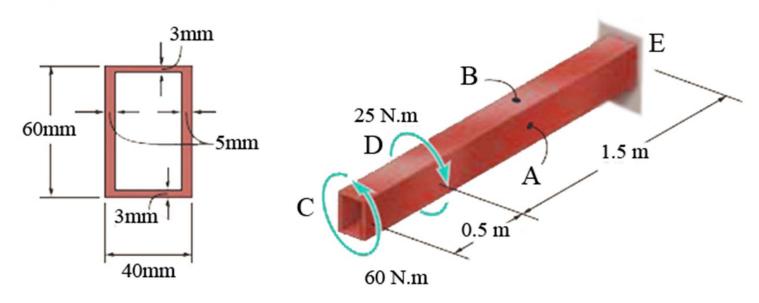




Example 5

The tube is made of C86100 bronze and has a rectangular cross section as shown below. If it is subjected to the two torques, determine the average shear stress in the tube at points A and B. Also, what is the angle of twist of end C? The tube is fixed at E.

(a)



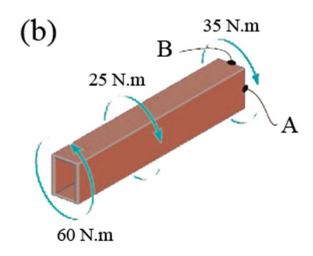


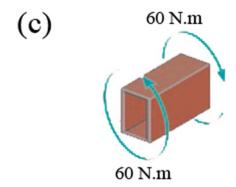
Example 5 (cont.)

$$A_m = (0.035)(0.057) = 0.002 \text{ m}^2$$

$$\tau_A = \frac{T}{2tA_m} = \frac{35}{2(0.005)(0.002)} = 1.75 \text{ MPa}$$

$$\tau_B = \frac{T}{2tA_m} = \frac{35}{2(0.003)(0.002)} = 2.92 \text{ MPa}$$

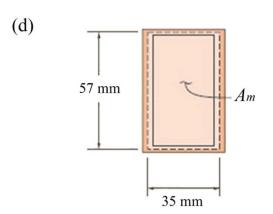


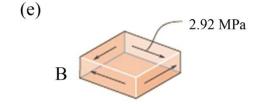


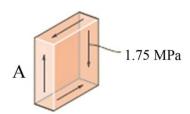


Example 5 (cont.)

$$\varphi = \frac{TL}{4A_m^2 G} \oint \frac{ds}{t} = \frac{60(0.5)}{4(0.002)^2 \left[38(10^9)\right]} \left[2\left(\frac{57}{5}\right) + 2\left(\frac{35}{3}\right)\right] + \frac{35(1.5)}{4(0.002)^2 \left[38(10^9)\right]} \left[2\left(\frac{57}{5}\right) + 2\left(\frac{35}{3}\right)\right] = 6.29(10^{-3}) \text{ rad}$$











References

- 1. Hibbeler, R.C., Mechanics Of Materials, 8th Edition in SI units, Prentice Hall, 2011.
- Gere dan Timoshenko, Mechanics of Materials, 3rd Edition, Chapman & Hall.
- Yusof Ahmad, 'Mekanik Bahan dan Struktur' Penerbit UTM 2001